

Review on Dimpled andProtruded Roughness Geometries used in the Duct of Solar Air Heaters

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ABSTRACT

Application of artificial roughness is considered to be an effective technique for improving thermal performance of a solar air heater (SAH). Different types of roughness geometries have been reported in the literature. Among those, the most promising geometries are in the fabrication of dimples and protrusions on the absorber plate. In this paper, an attempt has been made to review the dimpled and protruded roughness geometries used in the duct of SAHs and Nusselt number (Nu) and friction factor (f) correlations developed by various investigators. Comparative study of the thermohydraulic performance of dimpled and protruded roughness geometries has also been reported and discussed in this paper.

Keywords: Friction factor, Roughened duct, Nusselt number, Solar air heater,

I. INTRODUCTION

The demand and consumption of energy have been increasing multifold due to increase in world population, boom in industries, improving the living standard and economic upbeat. World is heading towards global energy crisis due to degeneration in the availability of prime energy resources i.e. fossil fuels. Large-scale use of primary energy sources has also created a serious problem of environmental degradation which has been deteriorating human health very dangerously. Release of a lot of harmful gases into the atmosphere also resulted in acid raining, global warming etc. Now, another energy sources and especially the renewable energy (RE) sources are fascinating the courtesy of inventors and researchers. Out of many RE sources, solar energy is an important and promising renewable energy source which is available freely, non-polluting and massive potential of fulfilling all energy needs. Solar energy has many applications like crop drying, domestic and industrial heating, ventilation and air conditioning (HVAC) system [1]. Solar collector is a special kind of heat exchanger that transforms solar energy into thermal energy. In solar collectors, solar air heater is to be considered as cheap, simple in construction and having various advantages in comparison to solar water heater like corrosion and freezing free [2]. The thermal efficiency of SAH is less because of the low rate of heat transfer between the absorber plate and air flowing in the duct of SAH [3]. Thermal performance of solar air heater can be improved by enhancing the convective heat transfer coefficient with the use of artificial roughened absorber plates [4-5]. Various authors have carried out a critical review of different rib geometries used for creating an artificial roughness on absorber plate of aSAH [6-9]. Authors have



reported the concept of artificial roughness in the literature and first-time use of artificial roughness in heat exchanger devices [10]. Among different techniques of creating an artificial roughness on the surface of absorber plate of solar air heater duct, the formation of dimples and protrusions is considered to be simple, an innovative and economic technique [11]. In this paper, an attempt has been made to review the dimpled and protruded roughness geometries used in the duct of SAHs and Nu and f correlations developed by various investigators. Comparative study of the thermohydraulic performance of dimpled and protruded roughness geometries has also been reported and discussed in the present paper.

II. CONCEPT OF ARTIFICIAL ROUGHNESS

Thermal performance of SAH is poor because of the low rate of heat transfer between the absorber plate and air flowing through the duct of SAH. In order to make SAHs parsimoniously viable, their thermal efficiency needs to be enhanced by augmenting the heat transfer coefficient. In order to achieve higher heat transfer coefficient, it is desirable that the laminar sub-layer formed on the surface of absorber plate during the flow of air should be broken and flow at the heat transferring surface is made turbulent. This can be achieved by providing artificial roughness on the surface of absorber plate [3-5]. However, with roughened absorber plate, excessive power is required to make the flow of air through the duct. In order to avoid excessive friction loss, flow of air should not be unduly disturbed. It is therefore desirable that turbulence must be generated only in laminar sublayer region which is very close to the heat transferring surface. It can be done by keeping the height of the roughness element small in comparison with the duct dimension [3-9].

III. DIMPLED AND PROTRUDED ROUGHNESS GEOMETRIES USED IN SOLAR AIR HEATER

Formation of dimples and protrusions on the surface of absorber plate to create artificial roughness is considered to be simple, an innovative and economic technique. It has been observed that in dimpled and protruded roughness geometries, friction penalty is less as compared to heat transfer enhancement [6]. Various types of dimpled and protruded roughness geometries used in the SAH ducts, reported by various investigators have been presented and discussed in the present section.

3.1 Dimpled roughness geometry

Saini and Verma [12] studied the effect of parameters on heat transfer and friction characteristics in a roughened duct provided with dimpled roughness geometry as shown in Fig.1 for Reynolds number (Re) range of 2000-12,000. The range of relative roughness height (e/D) of 0.018-0.037 and relative roughness pitch (P/e) of 8-12 respectively. Authors reported that Nu and f augmented by 1.8 and 1.4 times as compared to the smooth duct. Nu and f correlations as function of Re for roughened duct were recommended as follows;

$$\begin{aligned} Nu &= 5.2 \times 10^{-4} Re^{1.27} (p/e)^{3.15} \\ &\times \left[\exp(-2.12) (\log(p/e))^2 \right] (e/D)^{0.033} \\ &\times \left[\exp(-1.30) (\log(e/D))^2 \right] \end{aligned} \quad (1)$$

$$f_r = 0.642 \text{Re}^{-0.423} (p/e)^{-0.465} \times \left[\exp(0.054) (\log(p/e))^2 \right] (e/D)^{-0.0214} \times \left[\exp(0.840) (\log(e/D))^2 \right] \quad (2)$$

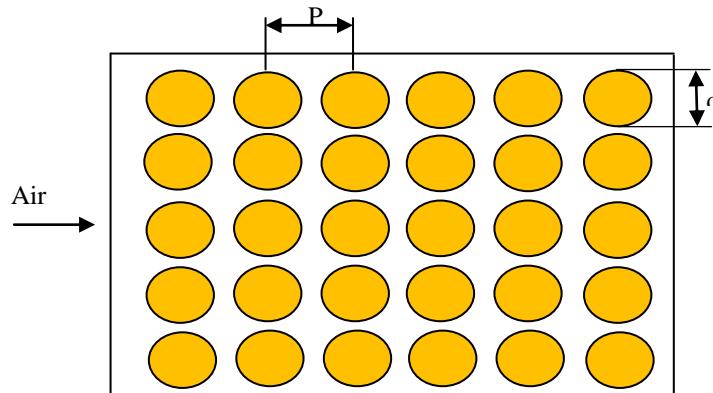


Fig. 1. Absorber plate having dimpled roughness

Sethi et al. [13] studied the effect of dimple arranged in an angular arc shape as shown in Fig. 2 for Re range of 3600-18,000. The range of relative roughness pitch (P/e) of 10-20, relative roughness height (e/D) of 0.021-0.036 and arc angle (α) of 45° - 75° respectively. Maximum enhancement in Nu and f as 2.54 and 3 times in comparison to the smooth duct has been reported by the authors. Nu and f correlations as function of Re for roughened duct were recommended as follows;

$$\begin{aligned} Nu &= 7.1 \times 10^{-3} \times \text{Re}^{1.1386} \times (e/D_h)^{0.3629} \\ &\times (p/e)^{-0.047} \times (\alpha/60)^{-0.0048} \\ &\times \exp[-0.7792(\ln(\alpha/60))^2] \end{aligned} \quad (3)$$

$$\begin{aligned} f &= 4.869 \times 10^{-1} \times (e/D_h)^{0.2663} \times \text{Re}^{-0.233} \\ &\times (p/e)^{-0.059} \times (\alpha/60)^{0.0042} \\ &\times \exp[-0.4801(\ln(\alpha/60))^2] \end{aligned} \quad (4)$$

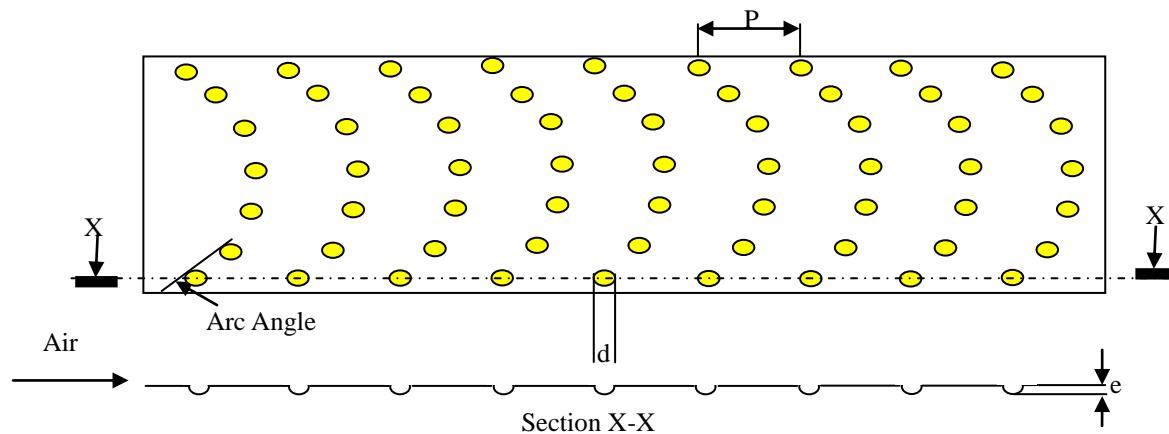


Fig. 2. Absorber plate having dimple arranged in an angular arc shape.

Kumar et al. [14] studied the effect of multiple V-pattern dimples as roughness geometry as shown in Fig. 3 for Re range of 5000-17,000. Range of relative dimpled obstacles width (W_c/W_d), dimpled depth to print diameter (e_d/d_d), relative dimpled pitch (P_b/e_d), 8.0-11.0 and angle of attack (α_a) was 1.0-6.0, 0.50-2.0, 8.0-11.0 and 35°-75° with fixed relative dimpled height (e_d/D_h) of 0.037 respectively. Maximum enhancement in Nu and f as 6.4 and 8 times in comparison to the smooth duct has been reported by the authors. Nu and f correlations as function of Re for roughened duct were recommended as follows;

$$\begin{aligned} Nu = & 9.35 \times 10^{-14} Re^{1.065} (W_c / W_D)^{2.9832} \times (P_b / e_d)^{2.99} \\ & \times (e_d / D_d)^{-0.248} \times (\alpha / 55)^{-0.096} \\ & \times \exp \left[(-0.91) \ln \left(\frac{W_c}{W_d} \right)^2 \right] \times \exp \left[\ln \left(\frac{P_b}{e_d} \right)^2 \right] \\ & \times \exp \left[(-0.1906) \ln \left(\frac{e_d}{D_d} \right)^2 \right] \\ & \times \exp \left[(-2.563) \ln \left(\frac{\alpha}{55} \right)^2 \right] \end{aligned} \quad (5)$$

$$\begin{aligned} f = & 2.05 \times 10^{-5} Re^{-0.6307} (W_c / W_D)^{0.0853} \times (P_b / e_d)^{19.13} \\ & \times (e_d / D_d)^{-0.162} \times (\alpha / 55)^{-0.2254} \\ & \times \exp \left[(0.0676) \ln \left(\frac{W_c}{W_d} \right)^2 \right] \times \exp \left[\ln \left(\frac{P_b}{e_d} \right)^2 \right] \\ & \times \exp \left[(-0.341) \ln \left(\frac{e_d}{D_d} \right)^2 \right] \\ & \times \exp \left[(-2.303) \ln \left(\frac{\alpha}{55} \right)^2 \right] \end{aligned} \quad (6)$$

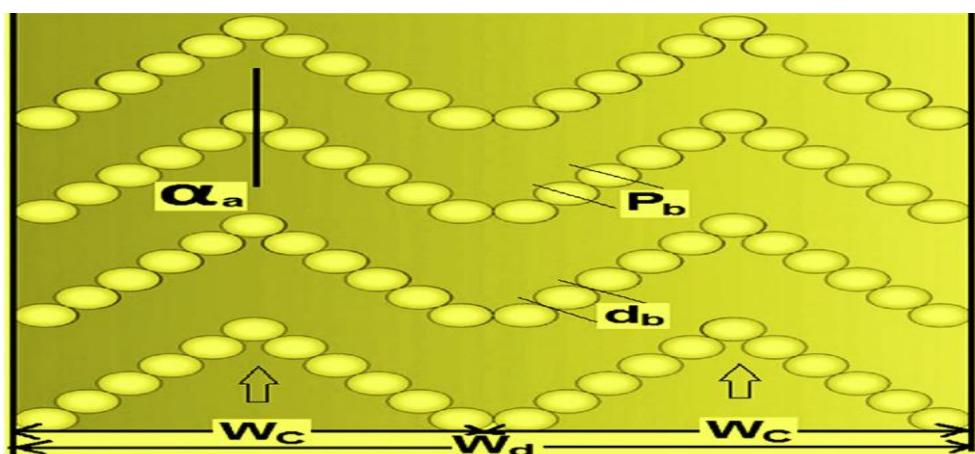


Fig. 3. Absorber plate having dimple arranged in multiple V-pattern shape.



3.2 Roughness geometry in the form of protrusions

Bhushan and Singh [11] carried out an experimental investigation on heat transfer and friction characteristics of a roughened duct having protruded roughness geometry provided on absorber plate as shown in Fig. 4 for Re range of 4000-20,000. The range of relative short way length(S/e) of 18.75-37.50 and relative long way length(L/e) of 25.0-37.5 with fixed relative roughness height (e/D) of 0.03. Maximum improvement in Nu and f as 3.8 and 2.2 times in comparison to the smooth duct has been reported by the authors. Nu and f correlations as function of Re for roughened duct were recommended as follows;

$$Nu = 2.1 \times 10^{-88} Re^{1.452} (S/e)^{12.94} (L/e)^{99.2} (d/D)^{-3.9} \times \exp\left[(-10.4)\{\log(S/e)\}^2\right] \times \exp\left[-77.2\{\log(L/e)\}^2\right] \times \exp\left[(-7.83)\{\log(d/D)\}^2\right] \quad (7)$$

$$f = 2.32 Re^{-0.201} (S/e)^{-0.383} (L/e)^{-0.484} (d/D)^{0.133} \quad (8)$$

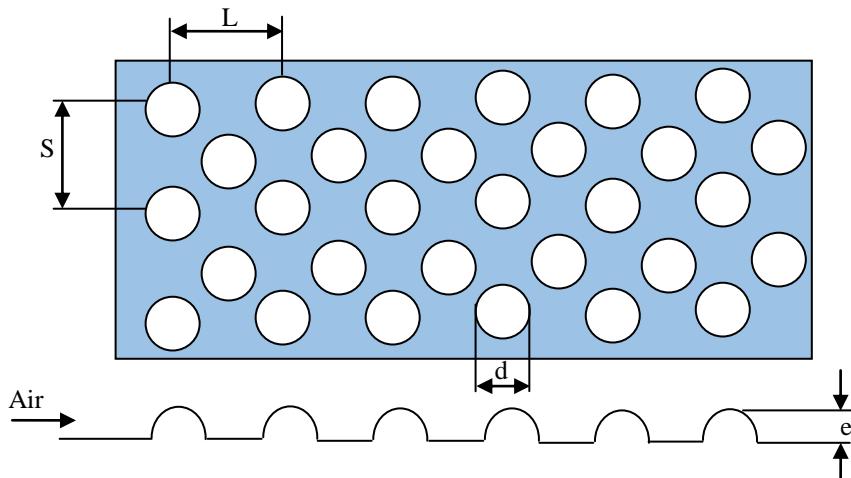


Fig. 4. Absorber plate roughened with protruded shaped geometry.

Yadav et al. [15] reported an experimental investigation on heat transfer and friction characteristics of SAH duct having protrusions arranged in an arc shape on absorber plate as shown in Fig.5 for Re range of 3600-18,100. The range of e/D, P/e and α was 0.015- 0.03, 12-24 and 45° - 75° respectively. Authors reported maximum enhancement in heat transfer and friction factor as 2.89 and 2.93 times in comparison to the smooth duct for the investigated range of parameters. Nu and f correlations as function of Re for roughened duct were recommended as follows;

$$Nu = 0.154 \times Re^{1.017} \times (p/e)^{-0.38} \times (e/D)^{0.521} (\alpha/60)^{-0.213} \times \exp\left(-2.023(\ln(\alpha/60))^2\right) \quad (9)$$

$$f = 7.207 \times Re^{-0.56} \times (p/e)^{-0.18} \times (e/D)^{0.176} (\alpha/60)^{0.038} \times \exp\left(-1.412(\ln(\alpha/60))^2\right) \quad (10)$$

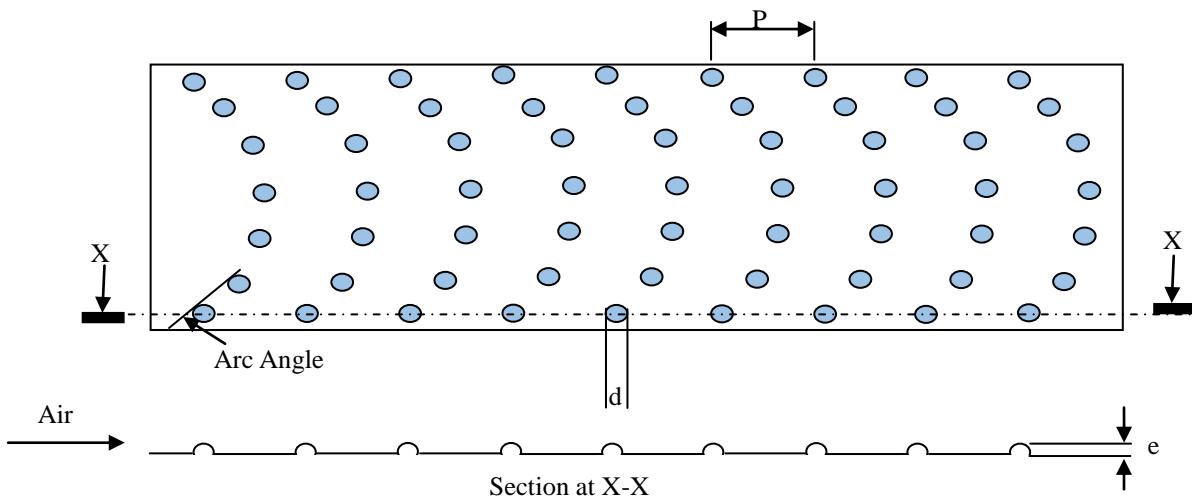


Fig. 5. Absorber plate roughened with protruded shaped arranged in angular arc.

IV. COMPARISON OF DIMPLED AND PROTRUDED ROUGHNESS GEOMETRY

It is required that design of solar airheater should be made in such a way that heat transfer should be maximum with minimum power requirement [6]. In order to bring into account the power required for propelling air through the duct, it is more appropriate to evaluate thermohydraulic performance instead of evaluating the thermal performance of a solar air heater. In the present paper, thermohydraulic performance has been evaluated by using the following relationship reported by Jaurker et al. [16].

$$\eta = \frac{Nu / Nu_s}{(f / f_s)^{\frac{1}{3}}} \quad (11)$$

where η = efficiency index

Nu = Nusselt number (roughened duct)

Nu_s = Nusselt number (smooth duct)

f = friction factor (roughened duct)

f_s = friction factor (smooth duct)

Comparison of thermohydraulic performance of dimple and protrusion roughness geometries investigated by different authors has been shown in Fig.6. Thermohydraulic performance has been compared evaluated by using the Nu and f correlations for dimple and protrusion roughness geometries.

It can be observed from Fig. 6 that protruded roughness geometry resulted better thermohydraulic performance as compared to that has been resulted by dimpled roughness geometry for the investigated range of parameters.

V. CONCLUSIONS

In this paper, an attempt has been made to review the dimpled and protruded roughness geometries being used to enhance the thermal performance of SAHs.

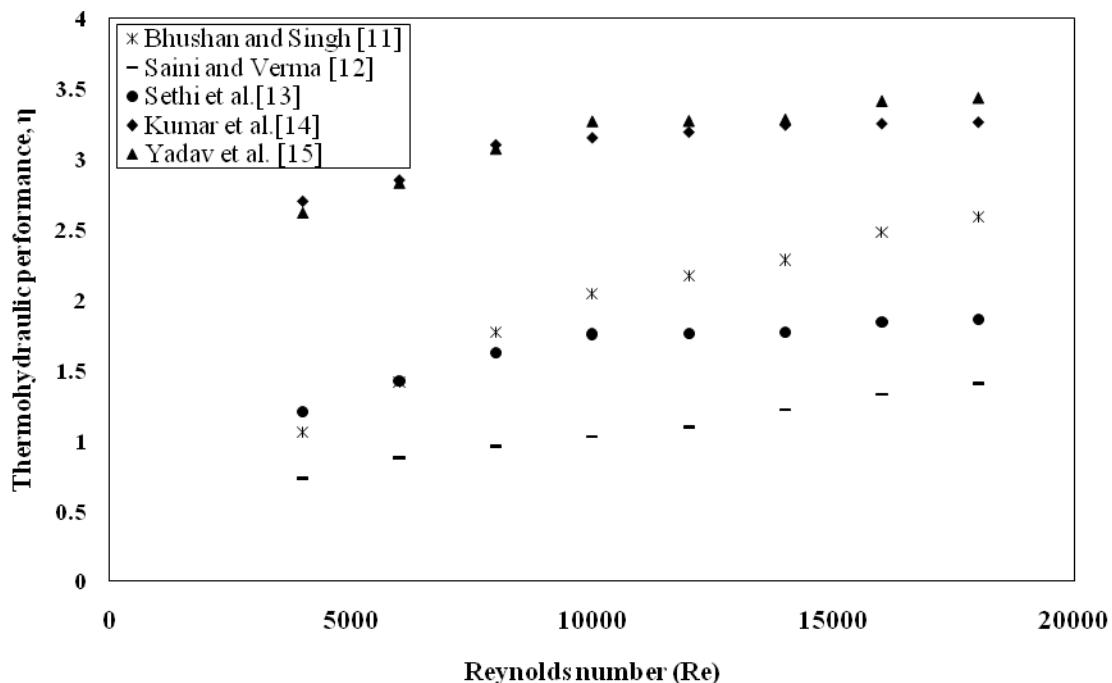


Fig.6. Comparison of thermohydraulic performance of ductroughened with dimples and protrusions.

It is found from the literature that formation of dimples or protrusions on the surface of absorber plate of a solar air heater is considered to be an innovative, simple and an economic technique. Nusselt number and friction factor correlations developed by various investigators for dimpled and protruded roughness geometries have also been reported in this paper. Comparison of thermohydraulic performance of SAH ducts having dimpled and protruded roughness geometries have shown that protruded roughness geometry results in a better thermohydraulic performance.

REFERENCES

- [1] S.P. Sukhatme,*Solar Energy: Principles of Thermal Collection and Storage*,(9th Ed. Tata McGraw-Hill2003), New Delhi.
- [2] J.A. Duffie and W.A. Beckman, *Solar Engineering of Thermal Processes* (Wiley,1980),New York.
- [3] A. Soi, R. Singh and B. Bhushan, CFD based performance investigation of solar air heater having roughness elements as a combination of transverse & V-up ribs on the absorber plate, *International Journal of Advance Research in Science and Engineering*, 4 (01), 2015, 1700-1709.
- [4] Varun,R.P. Saini, and S.K. Singal.,A review on roughness geometry used in solar air heaters. *Solar Energy*, 81, 2007, 1340-1350.
- [5] V.S. Hans, R.P. Saini, and J.S. Saini,Performance of artificially roughened solar air heaters- a review,*Renewable and Sustainable Energy Reviews*, 13, 2009,1854-1869.
- [6] B. Bhushan, and R. Singh,A review on methodology of artificial roughness used in duct of solar air heaters,*Energy*, 35, 2010,202-212.
- [7] A.M. Lanjewar, J.L. Bhagoria, and M.K. Agrawal,Review of development of artificial roughness in solar

air heater and performance evaluation of different orientations for double arc rib roughness,*Renewable and Sustainable Energy Reviews*, 43, 2015, 1214-1223.

- [8] A.S. Yadav, and M.S. Thapak,Artificially roughened solar air heater: experimental investigations,*Renewable and Sustainable Energy Reviews*, 36, 2014, 370-411.
- [9] T. Alam and M.H. Kim,A critical review on artificial roughness in rectangular solar air hater duct,*Renewable and Sustainable Energy Reviews*, 69, 2017, 387-400.
- [10] A.E. Bergles, R.L. Webb and G.H. Junkan, Energy conservation via heat transfer enhancement,*Energy*, 41, 1979, 93-200.
- [11] B. Bhushan and R. Singh,Nusselt number and friction factor correlations for solar air heater duct having artificial roughened absorber plate, *Solar Energy*, 85, 2011, 1109-1118.
- [12] R.P. Sainiand J. Verma,Heat transfer and friction factor correlations for a duct having dimple-shape artificial roughness for solar air heaters,*Energy*,33, 2008,1277–1287.
- [13] M. Sethi, Varunand N.S. Thakur,Correlations for solar air heater duct with dimpled shape roughness elements on absorber plate, *Solar Energy*, 86, 2012,2852-2861.
- [14] A.Kumar, R. Kumar, R. Maithani,R. Chauhan,M. Sethi,A. Kumari,S.Kumar and S. Kumar, Correlation development for Nusselt number and friction factor of a multiple type V-pattern dimpled obstacles solar air passage, *Renewable Energy*, 109, 2017, 461-479.
- [15] S.Yadav, M.Kaushal, Varun and Siddhartha,Nusselt number & friction factor correlations for solar air heater duct having protrusions as roughness elements on absorber plate, *Experimental Thermal and Fluid Science*, 44, 2013, 34-41.
- [16] A. R. Jaurker, J.S. Saini and B.K.Gandhi, Heat transfer and friction characteristics of rectangular solar air heater duct using rib-grooved artificial roughness, *Solar Energy*, 80 (8), 2006, 895–907.