

# TRANSFORMER OVERLOAD PROTECTION

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## ABSTRACT

This paper presents a way to sought out the problem of transformer overload by keeping the problem of biggest power failure all over the world in mind. It is possible to design transformer protection relay that detect overload condition based on calculated hot spot temperature. It contain all the transmission subject: a) transmission design b) hot spot detection ( transmission diagnostic) c) transmission failure d) overload protection

**Keywords – Connection, Design, Diagnostic, Overload, Power Failure, Transformer**

## I INTRODUCTION

Transformer is basically defined as a a static electrical device that transfers energy by inductive coupling between its winding circuits. A transformer plays a very critical role in our daily routine life. In the short span of two centuries electrical power has become an indispensable part of modern day life. Our work, leisure, healthcare, economy, and livelihood depends on a constant supply of electrical power. Even a temporary stoppage of power can lead to relative chaos, monetary setback and possible loss of life, decrease in productivity, loss revenue. There are many causes of power failure and to protect ourselves from its adverse devastating effect one should know about its main causes:

Natural cause (70% of power outage 2)Other cause ( 11%) 3) Short circuit 4)Overloading 5)Power surge

Here in this paper we are dealing with only transformer overload and requirement of overload protection. We think it is better to install transformer overload relay to protect ourselves from the great failures.

### 1.1 Power outages:

**Power outage means it should conform he following criteria:**

- i. The outage must not be planned by the service provider.
- ii. The outage must affect at least 1,000 people and last at least one hour.
- iii. There must be at least 1,000,000 person- hours of disruption.

The table below shows some of the largest power outages:

| Article                           | Millions people affected | Location   | Date                | Reference |
|-----------------------------------|--------------------------|--|---------------------|-----------|
| July 2012 India blackout          | 670                      | India  | 30-31 july 2012     | [1]       |
| 2005 Java-Bali blackout           | 100                      | Indonesia  | 18 august 2005      | [2]       |
| 1999 southern brazil blackout     | 99                       | Brazil   | 11 march 1999       | [3]       |
| 2009 Brazil and Paraguay blackout | 87                       | Brazil and Paraguay                                  | 10-11 november 2009 | [4]       |
| Northeast blackout 2003           | 55                       | The united states<br>Canada                          | 14-15 august 2003   | [5]       |
| Italy blackout 2003               | 55                       | Italy, Switzerland,<br>Austria, Slovenia,<br>Croatia | 28 september 2003   | [6]       |
| Northeast blackout 1965           | 30                       |  | 9 november 1965     | [7]       |

## 1.2 Transformer Protection Principles

The type of protection for the transformers varies depending on the application and the importance of the transformer. Transformers are protected primarily against faults and overloads. The type of protection used should minimize the time of disconnection for faults within the transformer and to reduce the risk of catastrophic failure to simplify eventual repair. Any extended operation of the transformer under abnormal condition such as faults or overloads compromises the life of the transformer, which means adequate protection should be provided for quicker isolation of the transformer under such conditions

## 1.3 Transformer Failures

Failures in transformers can be classified into

- i. Winding failures due to short circuits (turn-turn faults, phase-phase faults, phase-ground, open winding)
- ii. Core faults (core insulation failure, shorted laminations)
- iii. Terminal failures (open leads, loose connections, short circuits)
- iv. On-load tap changer failures (mechanical, electrical, short circuit, overheating)

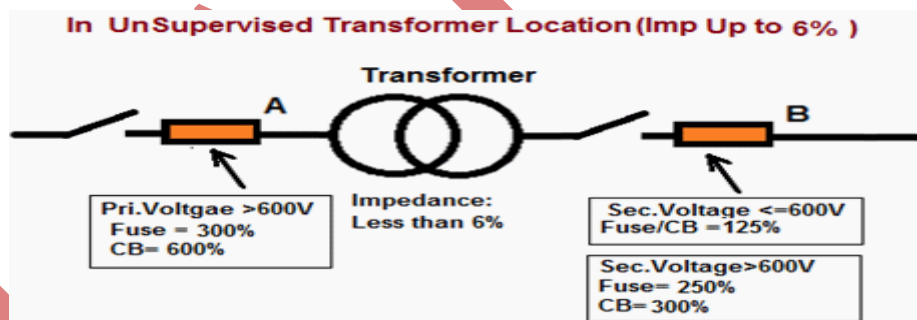
| Conditions                               | Protection Philosophy  |
|--|--|
| <b>Internal</b>                          |  |
| Winding Phase-Phase, Phase-Ground faults | Differential (87T), over current (51, 51N)<br>Restricted ground fault protection (87RGF) |
| Winding inter-turn faults                | Differential (87T), Buchholz relay,  |

|  |   |
|--|---|
| Core insulation failure, shorted laminations | Differential (87T), Buchholz relay, sudden pressure relay         |
| Tank faults                                  | Differential (87T), Buchholz relay and tank-ground protection     |
| Over fluxing                                 | Volts/Hz (24)   |
| <b>External</b>                              |   |
| Overloads                                    | Thermal (49)  |
| Overvoltage                                  | Overvoltage (59)  |
| Over fluxing                                 | Volts/Hz (24)   |
| External system short circuits               | Time over current (51, 51G), Instantaneous over current (50, 50G) |

## II OVER CURRENT PROTECTION OF TRANSFORMER (NEC 450.3)

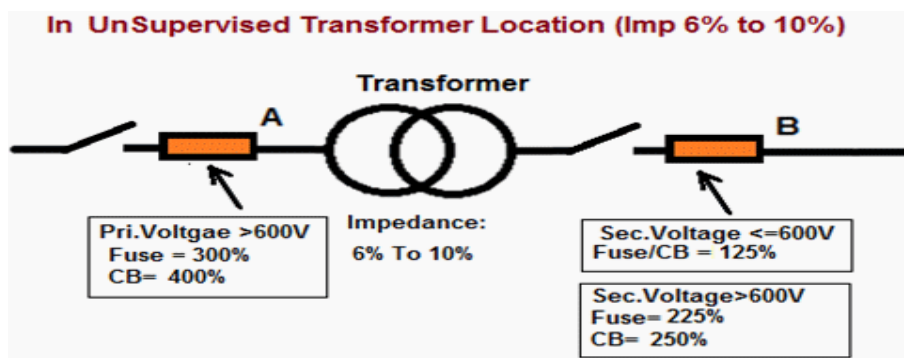
The over current protection required for transformers is consider for protection of transformer only. Such over current protection will not necessarily protect the primary or secondary conductors or equipment connected on the secondary side of the transformer.

### 2.1 Unsupervised Location of Transformer (Impedance <6%)



- i. Over Current Protection at Primary Side (Primary Voltage >600V)
- ii. Rating of Pri. Fuse at Point A= 300% of Pri. Full Load Current or Next higher Standard size. or
- iii. Rating of Pri. Circuit Breaker at Point A= 600% of Pri. Full Load Current or Next higher Standard size.
- iv. Over Current Protection at Secondary Side (Secondary Voltage ≤600V):
- v. Rating of Sec. Fuse / Circuit Breaker at Point B= 125% of Sec. Full Load Current or Next higher Standard size.
- vi. Over Current Protection at Secondary Side (Secondary Voltage >600V):
- vii. Rating of Sec. Fuse at Point B= 250% of Sec. Full Load Current or Next higher Standard size. Or Rating of Sec. Circuit Breaker at Point B= 300% of Sec. Full Load Current.

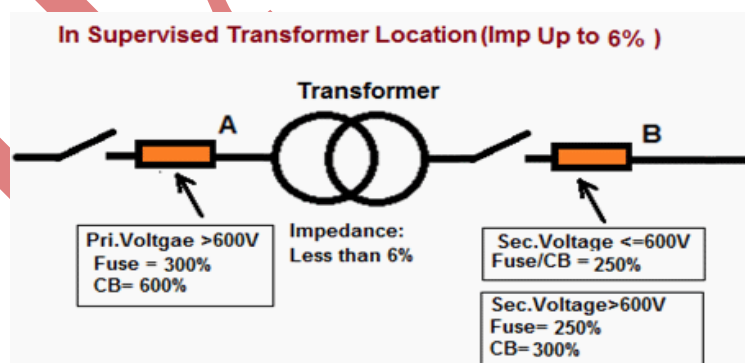
## 2.2 Unsupervised Location of Transformer (Impedance 6% to 10%)



### Unsupervised Location of Transformer (Impedance 6% to 10%)

- i. Over Current Protection at Primary Side (Primary Voltage >600V):
- ii. Rating of Pri. Fuse at Point A= 300% of Primary Full Load Current or Next higher Standard size.
- iii. Rating of Pri. Circuit Breaker at Point A= 400% of Primary Full Load Current or Next higher Standard size.
- iv. Over Current Protection at Secondary Side (Secondary Voltage <=600V):
- v. Rating of Sec. Fuse / Circuit Breaker at Point B= 125% of Sec. Full Load Current or Next higher Standard size.
- vi. Over Current Protection at Secondary Side (Secondary Voltage >600V):
- vii. Rating of Sec. Fuse at Point B= 225% of Sec. Full Load Current or Next higher Standard size.
- viii. Rating of Sec. Circuit Breaker at Point B= 250% of Sec. Full Load Current or Next higher Standard size.

## 2.3 Supervised Location of Transformer (Impedance Up to 6%)



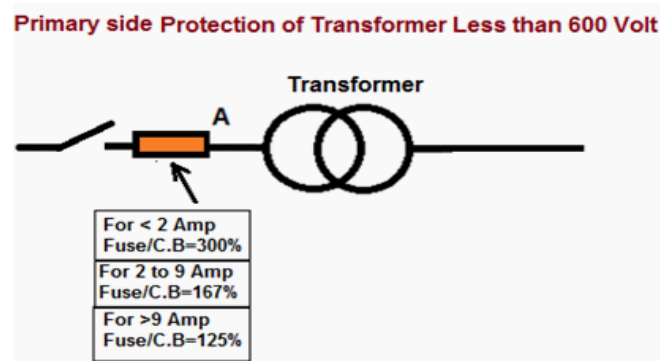
- i. Over Current Protection at Primary Side (Primary Voltage >600V):
- ii. Rating of Pri. Fuse at Point A= 300% of Pri. full load current or next lower standard size.
- iii. Rating of Pri. Circuit Breaker at Point A= 600% of Pri. full load current or next lower standard size.
- iv. Over Current Protection at Secondary Side (Secondary Voltage <=600V):



**NH: Next Higher Standard Size.**

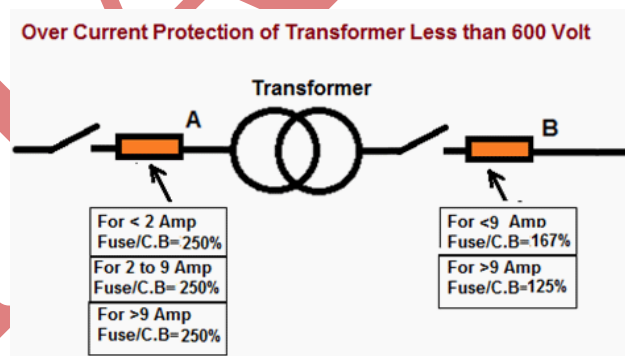
## Over current Protection of transformers <600V (NEC 450.3B)

### 3.1 Only Primary Side Protection of Transformer



- i. Over Current Protection at Primary Side (Less than 2A):
- ii. Rating of Pri. Fuse / C.B at Point A = 300% of Pri. full load current or next lower standard size.
- iii. Example: 1KVA, 480/230 3Phase transformer, full load current at Pri. side =  $1000/(1.732 \times 480) = 1A$
- iv. Rating of Primary Fuse =  $3 \times 1A = 3A$ , so next lower standard size of Fuse = 3A.
- v. Over Current Protection at Primary Side (2A to 9A):
- vi. Rating of Sec. Fuse / C.B at Point A = 167% of Pri. full load current or next lower standard size.

### 3.2 Primary and Secondary side Protection of Transformer



Over Current Protection at Primary Side (Less than 2A):

- i. Rating of Pri. Fuse / C.B at Point A = 250% of Pri. full load current or next lower standard size.
- ii. Over Current Protection at Primary Side (2A to 9A):
- iii. Rating of Sec. Fuse / C.B at Point A= 250% of Pri. full load current or next lower standard size.
- iv. OverCurrent Protection at Primary Side (More than 9A):

- v. Rating of Pri. Fuse / C.B at Point A= 250% of Pri. Full Load Current or Lower Higher Standard size.

#### IV SUMMARY OF OVER CURRENT PROTECTION FOR LESS THAN 600V

| Maximum Rating of Overcurrent Protection for Transformers Less than 600 Volts |                    |          |              |                      |              |
|---|--------------------|----------|--------------|----------------------|--------------|
| Protection Method   | Primary Protection |          |              | Secondary Protection |              |
|   | More than 9A       | 2A to 9A | Less than 2A | More than 9A         | Less than 9A |
| Primary protection only   | 125%(NH)           | 167%     | 300%         | Not required         | Not required |
| Primary and secondary protection  | 250%               | 250%     | 250%         | 125%(NH)             | 167%         |

#### V CONCLUSION

It is possible to design transformer protection relay that detect overload condition based on calculated hot spot temperature and react in an intelligent way. This paper describes some of the largest power failures, transformer protection principle, transformer failures.

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